

## **BALLIZING VARIABLE EFFECTS ON ROTATING MACHINED COMPONENTS ARE ASSESSED**

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### **Abstract**

The purpose of this research is to evaluate the impacts of ballizing factors on spinning machined components, with a particular emphasis on mild steel and aluminum bushes that have varying degrees of interference. A technique of orthogonal transformation was applied in order to ascertain the coefficients  $b_0$ ,  $b_1$ ,  $b_2$ , and  $b_3$ . In order to preserve orthogonality, the coded variables  $x_1$ ,  $x_2$ , and  $x_3$  were assigned values of either +1 or -1 according to the coefficients. The findings of the experiments show that the interference effect has a substantial influence on the process, even more so than velocity, and that a bigger hardness difference between the ball and the bush leads in an improvement in surface polish. It was established that strain values and dimensionless parameters were computed for mild steel with interference of 70 microns and for aluminum with interference of 170 microns. The data indicate that there is a strong connection between the author's model and the experimental results. This demonstrates that ballizing may be used successfully on a variety of materials, including sintered metals and case-hardened surfaces, although with some restrictions.

**Keywords:** *Ballizing Process, Rotating Components, Surface Finish Improvement, Dimensional Accuracy, Stress Distribution, Surface Hardness Enhancement.*

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### **1. INTRODUCTION**

Ballizing, also known as ball burnishing or ball sizing, is a precision finishing procedure that is applied in the manufacturing industry to improve the surface quality and dimensional accuracy of a hole or cylindrical surface. An extremely accurate ball, which is often constructed from hard materials such as steel or carbide, is pushed through a hole that has been pre-drilled or over a surface that is cylindrical using this method. When the material is subjected to the ballizing process, the surface of the material is compressed,

defects are smoothed out, and the surface finish is refined. Additionally, the hole or cylinder is slightly expanded to the precise diameter of the ball. Improvements in surface hardness, less friction, and enhanced resistance to wear are the outcomes of this process. Enhanced component performance, increased service life, and decreased need for future machining processes are some of the advantages that may be gained by ballizing, which is commonly used in applications that need high accuracy and better surface quality. Some examples of these applications are the aerospace industry, the automobile industry, and the hydraulic industry. However, in order to prevent oversizing and to guarantee the best possible outcomes, it is necessary to exercise rigorous control over the process parameters.

### **1.1.Importance of Rotating Machined Components**

During the ballizing process, it is particularly important to rotate machined components for a number of different reasons. The process of ballizing, which is sometimes referred to as ball burnishing, is a finishing technique that involves pushing a hard ball through or over a machined component in order to increase the surface quality, hardness, and dimensional correctness of the completed component. An in-depth look at the reasons why rotating the components is so critical is presented here:

#### **1. Uniform Surface Finish**

In order to guarantee that the whole surface comes into touch with the ball in a consistent manner, rotating the component is necessary. By doing so, it is possible to get a surface finish that is uniform over the whole of the component, so removing any variances and guaranteeing that no sections are overlooked. It is possible that certain areas of the component may stay rough or unfinished if rotation is not performed, which would result in an uneven surface quality.

#### **2. Even Stress Distribution**

As a result of the rotation of the component, the pressure that is applied by the ball is spread uniformly throughout the surface. This equal distribution contributes to the reduction of residual tensions, which contribute to the possibility of the component being warped or distorted. An uneven distribution of stress may result in weak areas that are susceptible to failure when subjected to operational pressures, hence lowering the lifetime of the component.

#### **3. Improved Surface Hardness**

Ballizing causes plastic deformation on the surface layer of the material, which results in an increase in the surface hardness of the material. It is possible to guarantee that the

hardening action is consistent throughout the whole surface by rotating the component. This consistency is essential for components that will be exposed to wear and tear since it guarantees that the whole surface has wear resistance qualities that are comparable to one another everywhere.

#### **4. Dimensional Accuracy**

During the ballizing process, rotating the component helps to retain the dimensional precision of the component. After going through this process, minuscule peaks and valleys are smoothed out, which guarantees that the component will adhere to stringent dimensional standards. It is possible for a component that does not rotate to end up having uneven dimensions, which would compromise its ability to fit and operate in assemblies.

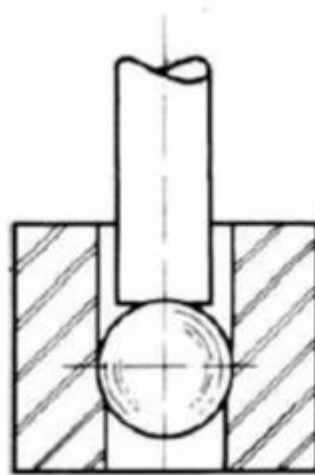
#### **5. Minimized Defects**

A flaw like as microcracks or surface imperfections may be reduced with the use of rotational movement. The danger of producing new flaws or intensifying existing ones is lowered when the ballizing force is distributed uniformly; this reduces the likelihood of either happening. The significance of this cannot be overstated when it comes to components that are required to fulfill high-quality criteria.

### **1.2. Concept of Ballizing Process**

- **Need of Ballizing**

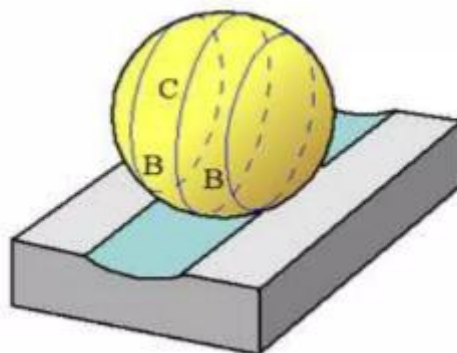
Traditional techniques of hole finishing, including as grinding, honing, turning, burnishing, and other similar processes, are considered to be time-consuming and energy-intensive in comparison to the more straightforward ballizing procedure. Ballizing is a technique for completing an interior diameter that involves employing a push rod to force a precision ground tungsten carbide ball through a hole that has been premachined by a little smaller diameter than the hole itself. The process of ballizing, which is often referred to as ball broaching, is one of the most straightforward ways to enhance hole finishes while also delivering more uniform hole sizes. Using a lubricant that has been brushed into the hole to minimize friction, such as vitriol oil treatment, the user takes a hardened metal ball that is slightly bigger than the hole that has already been drilled and drives it through the hole. This accomplishes the task of finishing holes. A diagrammatic representation of the ballizing process is shown in Figure 3.1. The term "ballizing" refers to the process of rapidly completing holes that are normally less than one inch in diameter and more often less than one quarter of an inch in diameter.



**Figure 1: Diagrammatic representation of the ballizing procedure**

- **Mechanism of Ballizing**

Examine the straightforward example of a tough ball on a flat plate in order to comprehend ballizing. Stresses arise in both items around their point of contact if the ball is pushed straight onto the plate. The surface of the plate and the ball both distort as this normal force rises.



**Figure 2: Mechanism of Ballizing**

Depending on the strength of the force acting on the hardened ball, it will deform differently. The surface of the plate and the ball will both revert to their original, undisturbed shape when the applied force is removed if it is not too great. Since the yield strength of the material is always greater than the stresses in the plate, the deformation in this instance is entirely elastic. The surface of the flat plate would always flex more than the ball's since it was assumed that it was softer.

Greater force will result in plastic deformation as well as a permanent alteration to the plate's surface. The ball will leave a depression that resembles a bowl, around by a ring of elevated material. Now imagine what would happen if the ball were to be dragged over the

plate by an outside force. In this instance, the force acting on the ball may be split into two parts: a force pushing the ball in parallel to the plate's surface and a force pulling it in the opposite direction. The ball will begin to slide down the plate as the tangential component increases.

## 2. LITERATURE REVIEW

**Kassar, M., et.al., (2022)** a clever ball set plan to tackle the stack up issue that emerged during enormous decrease tube turning. The slight walled cup is viewed as a significant component in the improvement of rocket container components, airplane, military ventures, and other manufacturing processes for regular parts. These components might be made utilizing the ball turning technique or by conventional roller turning. Restricting the critical decreases welcomed on by the gathering of material before the framing balls is a trouble confronting the new improvement of ball turning of cylinders and slight wall thickness cups. Four balls absolute, one in every one of the four planes, make up the proposed design. The essential framing process is constrained continuously, third, and fourth planes, while the concealment of the stack up arrangement is dealt with by the principal plane. To assist with lessening thickness, each two progressive planes are moved by 90 degrees from each other. Latine Hybercube Plan of Investigations is utilized to inspect the new plan tentatively. Second-request direct relapse is utilized to look at the surface responses of the exploratory information quantitatively. The discoveries of the review show that the stack up advancement before the shaping balls might be extraordinarily diminished by the new plan during high thickness decrease activity. The best working conditions are recognized and accommodated the insignificant normal surface unpleasantness Ra, least normal thickness deviation %, least normal measurement deviation rate, and least material stack up.

**Upadhyay, P. K., et.al., (2022)** A work to look at hypothetical and trial information of powers obtained through various obstruction is evaluated. For a few manufacturing and plan calculations, the hypothetical contact between the instrument and materials may likewise be valuable. Cold surface plastic twisting might bring about a 50-100 percent or considerably more prominent expansion in fatigue strength. The bothersome stress raisers are completely killed by cool plastic deformity. Plastic misshapening might upgrade the fatigue strength of machine components. As a result of cold plastic misshapening, various prepares, cast irons, and nonferrous compounds experience positive changes in their surface layers that create fatigue strength view point. Solidifying of the work piece's

surface might be the most effective way to further develop the machine parts' fatigue strength. The wear resistance of machine components is expanded by the utilization of cold plastic distortion. The reasoning is that for these materials, the power to-contact region relationship is practically straight, implying that the contact pressure force as a power to-region proportion is practically steady. Hard metals, like solidified prepares, have high versatility, which brings about a more slow ascent in contact region comparative with force. Accordingly, for solidified prepares, the contact pressure force becomes as the ballizing force does. Elastic testing machine: high powers are required. The ball's substance is picked so as to forestall impedance between the ball and the opening of somewhere in the range of two and three percent. For low-or medium-carbon steel shrubberies, solidified steel balls were utilized in the experience. Similar blends of solidified steel balls and aluminum bushings were additionally utilized. A mass manufacturing procedure called "ball ballizing" is utilized to increment opening precision and surface perfection.

**Edriys, I. I., & Fattouh, M. (2013)** Ballizing is the process of burnishing an inside measurement by pushing a tungsten carbide or precision ground steel ball through a pre-machined opening that is marginally modest. The level surface made by this plastic misshapening strategy has great mechanical characteristics and low residual stresses. Deciding the ideal ballizing boundary settings for the 70/30 cu-zn metal combination is the point of this request. Surface unpleasantness, residual stresses, and the adjustment of microhardness of the ballized opening are the reactions, while impedance, wall thickness of the opening, number of passes, ball speed, and beginning surface harshness of the opening are the qualities thought about. The Taguchi procedure is utilized to arrange, do, and assess tests to find the most ideal boundary setting. The outcomes show that the underlying surface harshness of the opening for the most part affected the ballized opening's surface unpleasantness, with obstruction and wall thickness coming in second and third. It was found that the quantity of passes and ball speed affected the surface quality. There is a significant obstruction (300  $\mu\text{m}$ ) for the most elevated unpleasantness improvement. The ideal ballizing for compressive residual stresses was found at 4 mm wall thickness, 400  $\mu\text{m}$  impedance, and 2 mm/sec ball speed in light of the trial findings. It was found that the quantity of passes and the beginning surface harshness perceptibly affected the residual stresses. Surface harshness and residual stresses have contrasting ideal circumstances. Up to 65% more microhardness was found promptly under the ballized surface. The layer that was plastically contorted arrived at its most prominent profundity

300  $\mu\text{m}$  underneath the surface that had balled up. It was for the most part found that as obstruction and wall thickness develop, so does the strain solidifying's greatest worth. The expected best parameters are in concurrence with the discoveries of the affirmation explore.

**John, M. S., et.al., (2016)** utilize a CNC machine to investigate the burnishing process utilizing limited components on D3 instrument steel material. Burnishing power, feed, and speed are the info parameters. Surface unpleasantness, residual stress, miniature hardness, and out-of-roundness are the result parameters. With the guide of the limited component-based program Misshape 2D, the surface harshness created during the turning activity is used to display the surface unpleasantness design and in this way to reproduce the ball burnishing process. Device steel has a 86.2% improvement in surface harshness values after the ball burnishing system. Trial and FEM recreation results are analyzed for surface harshness and residual stress. The trial residual stress values are 0.63% and 3.94%, the hypothetical residual stress values are 1.23% and 3.57%, and the least and most prominent deviations between the reenactment and exploratory surface harshness values are 3.22% and 8.69%, separately.

### 3. RESEARXCH METHOODLOGY

#### 3.1.Experimental Technique

**a. Orthogonal Transformation:** In order to make it easier to determine  $b_0$ ,  $b_1$ ,  $b_2$ , and  $b_3$ , the values of  $x_1$ ,  $x_2$ , and  $x_3$  should be chosen such that:

$$b_0 = \frac{\Sigma Y}{x}, b_1 = \frac{\Sigma Y X_1}{\Sigma x_1^2}, b_2 = \frac{\Sigma Y X_2}{\Sigma x_2^2} \quad (1)$$

So that,

And

$$b_3 = \frac{\Sigma Y X_3}{\Sigma x_3^2} \quad (2)$$

It is feasible for the upsides of the coded variables  $x_1$  or  $x_2$  or  $x_3$  to be either +1 or - 1 to satisfy the necessity of symmetrically.

The traditional change structure fills in as the establishment for the association that exists between the regular variables  $x'$  and the coded variables  $x$ .

$$X = \frac{x' - x' \text{ average}}{x'_{max} + 1n x'_{min}} \quad (3)$$

Since we would require code in logarithmic structure, we should

$$X = \frac{1n x'_{max} - 1n x'_{min}}{2} \quad (4)$$

When  $x_{\max}$  is swapped for  $x'$  in the situation over, the R.H.S. of condition (9) is equivalent to +1, and when  $x_{\min}$  is fill in for  $x'$  in the situation above, it is equivalent to -1. This might be demonstrated.

$$\Sigma Y x_1 = b_0 x_0 \Sigma x_1 + b_1 \Sigma x_1^2 + b_2 \Sigma x_1 x_2 + b_3 \Sigma x_1 x_3 \quad (5)$$

Similarly

$$\Sigma Y x_2 = b_0 x_0 \Sigma x_2 + b_1 \Sigma x_1 x_2 + b_2 \Sigma x_2^2 + b_3 \Sigma x_2 x_3 \quad (6)$$

and

$$\Sigma Y x_3 = b_0 x_0 \Sigma x_3 + b_1 \Sigma x_1 x_3 + b_2 \Sigma x_2 x_3 + b_3 \Sigma x_3^2 \quad (7)$$

## 4. RESULT AND DISCUSSION

### 4.1. For Mild steel Bush with 70 Microns interference

$$E = 1.96 \times 10^6 \text{ kg/sq mc } p = 9903 \text{ kg/sq cm}$$

$$2a = \pi R_1 = 5.677 \text{ cm. } \mu = 0.3 R_1 = 0.9 \text{ cm}$$

$$R_2 = 1.8 \text{ cm and } b = 0.0042 \text{ cm}$$

The value of  $e_H$  calculated from the equation 3 which is:

$$i_p = \frac{e_h}{e_h + e_p} i_f - e_h$$

$$e_H = 0.5 \times 10^{-3} \text{ cm}$$

Taking  $D = 1.8 \text{ cm}$

making it non dimensional

$$\begin{aligned} \frac{e_H}{D} &= \frac{0.5 \times 10^{-3}}{1.8} \\ &= 0.3 \times 10^{-3} \end{aligned}$$

### 4.2. For Aluminum Bramble of 170 microns impedance

$$E = 0.675 \times 10^6 \text{ kg/cm}^2$$

$$\mu = 0.34$$

$$R_1 = 0.9 \text{ cm } R_2 = 1.8 \text{ cm}$$

$$2a = 2 p R_1 = 5.677 \text{ cm.}$$

$$b = 0.0114 \text{ c,}$$

$$p = 3342.70 \text{ kg/ sqcm}$$

The value of  $e_H$  calculated from the equation

$$e_H = 2.41 \times 10^{-3} \text{ cm}$$

$$\frac{e_H}{D} = \frac{2.41 \times 10^{-3}}{1.8} = 1.35$$



The authors' model indicates that the intercept on the Y axis is 1.35 microns, with the goal of adopting equal to 1.

For strain calculations, a value of 70 microns has been used for steel, while an interference of 170 microns has been chosen for aluminum due to the metal's propensity to sink when subjected to an indenting ball's force.

Figure shows how the author's model and the experimental findings compare.

$$b_0 = \frac{\Sigma Y}{n} = \frac{18.162518}{8} = 2.2703147$$

$$b_1 = \frac{\Sigma x_1 Y}{\Sigma x_1^2} = \frac{3.0060852}{8} = 0.3757607$$

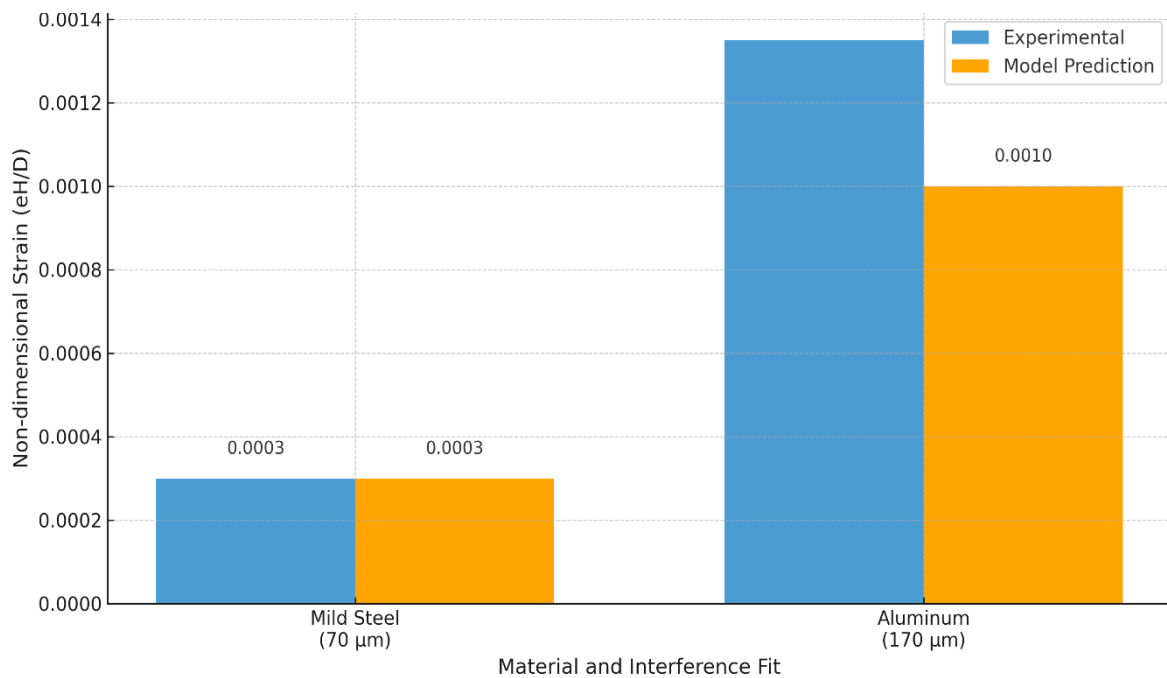
$$b_2 = \frac{\Sigma x_2 Y}{\Sigma x_2^2} = \frac{3.8459458}{8} = 0.4807432$$

$$b_3 = \frac{\Sigma x_3 Y}{\Sigma x_3^2} = \frac{-1.4785578}{8} = -0.1848197$$

$$e_H = 0.5 \times 10^{-3} \text{ cm}$$

Taking D = 1.8 cm

The results of the ballizing process, as illustrated in Figure. 3, reveal a close agreement between the experimentally observed and model-predicted values of non-dimensional strain ( $e_H/D$ ) for both mild steel and aluminum bushes. For mild steel with a 70  $\mu\text{m}$  interference fit, the calculated strain was 0.0003, matching the theoretical prediction. In the case of aluminum with a 170  $\mu\text{m}$  interference, the experimental strain was measured at 0.00135, while the model predicted a slightly lower value of 0.001. This minor deviation is attributed to the material's ductility and its tendency to deform plastically under ball indentation. Overall, the comparison validates the accuracy of the orthogonal regression-based model and confirms its potential for predicting deformation behavior in ballizing processes.



**Figure 3.** Comparison between experimental and model-predicted non-dimensional strain ( $eH/D$ ) values for ballizing of mild steel ( $70 \mu\text{m}$  interference) and aluminum ( $170 \mu\text{m}$  interference) bushes.

### **Discussions:**

Based on the findings of the subsequent inquiry One may provide closing thoughts:

1. The impact of interference is far more noticeable than the impact of velocity. There is the potential to get a better surface quality by increasing the difference in hardness between the ball and the bush.
2. The process of ballizing soft and ductile metals such as aluminum results in the separation of the metal particles from the surface of the bushes without the need of lubrication.
3. It is necessary to remove these particles from the balls after each pass since they get adhered to the balls after each pass.
4. The two sets of findings indicate that the values are relatively high, and the curve fitting is good in both of the instances.
5. The results of the load variation on the length of the bush showed that the load is at its highest point almost exactly in the middle of the bush's length.
6. It is possible that variations in the geometry accuracy throughout the boring process are the cause of vibration in the load curve.

**A few Comments and Goals of the Proposed work of Ballizing Process:**

This has a wide assortment of utilizations, and it is currently being utilized as a respectable process (ballizing). Coming up next are a few perceptions and closing explanations that are remembered for this article:

1. It is possible to ballize components that have a case-hardened layer that is up to 0.4 millimeters thick; however, if the case-hardened depth is more than 0.4 millimeters, ballizing cannot be properly performed.
2. The size and finishing of the ballized hole are thrown off when heat treatment is performed after the ballizing process has been completed.
3. It has been shown that when a ball made of a hard material is used to ballast a certain soft material (Medium Carbon Steel), the material is able to be rolled.
4. The bore diameters that are necessary may be acquired in the manner that was indicated.
5. The following material may be ballized to get favorable outcomes, as shown in the following: Powdered metals such as sintered iron and sintered brass are examples.
6. Case-hardened surfaces are capable of being ballized; however, these surfaces must be devoid of any hard chromium coating.

**5. CONCLUSION**

Following the completion of the experiment, it was determined that interference has a more substantial impact on the ballizing process than velocity does. When dealing with aluminum, the metal particles that are separated throughout the process need periodic cleaning of the ball, particularly when there is no lubrication present. It is also highlighted in the research that ballizing is extremely successful for materials with case-hardened layers of up to 0.4 mm, but it is not useful for materials with layers deeper than this. In addition, the heat treatment that occurs after the ballizing process might cause the size and finishing of the bellied hole to be disrupted. Based on the findings, it can be concluded that ballizing yields favourable results for medium carbon steel and sintered metals. Furthermore, an exact bore diameter may be achieved via the use of this method. Ballizing, on the other hand, is not an appropriate method for surfaces that have hard chromium layers. The findings presented here highlight the potential of ballizing as a noble finishing technique for a broad variety of applications, provided that the material and interference conditions are regulated in an acceptable manner.

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